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Minimal parameterization of fundamental matrices using motion and camera properties

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Abstract

This paper addresses the optimal recovery of the displacement and projection parameters from uncalibrated monocular video sequences. We study the particular cases of camera and objects displacements and camera projection in order to extract an optimized parameterization of the problem of parameters recovery for each cases.

This work follows previous studies on particular cases of displacement, scene geometry and camera analysis and focuses on the particular forms of fundamental matrices. This paper introduces the idea of using not all particular cases as individual cases but grouping these cases into a tractable number of sets, using properties on fundamental matrices.

Some experiments were performed in order to demonstrate that if several models are correct, the model with the least parameters gives the best estimate, corresponding to the true case. © 2002 Published by Elsevier Science B.V.

Keywords: Fundamental matrix; Particular displacement; Parameters estimation

1. Introduction

This paper deals with video sequences taken by an uncalibrated camera in an unknown environment. Our interest is to estimate as many parameters as possible on the camera and objects motion and the camera projection using a strategy of hypothesis testing.

Many efforts have been made in the Computer Vision community for determining motion and camera parameters from video sequences. Relations between 2D views exist [7] as the fundamental matrix \mathbf{F} , but, in the general case, we cannot extract all the unknown parameters from this \mathbf{F} matrix. It is however possible in some particular situations.

This work follows previous work on particular cases of displacement, scene geometry and camera analysis [10,11,18]. It focuses on the particular forms of fundamental matrices.

Several authors have already been interested in particular cases of projection [2,5,9,13,14,16] or displacement [3,4,8,17]. Some of them consider several cases and compare each result, in order to automatically determine which case was performed.

We call by general case the situation where we do not know anything about motion or camera projection. A particular case is when we know (or make the hypothesis) that a parameter is null, constant or known, or related to other parameters. A particular case has fewer parameters and/or simpler equations than the general one.

The motivations for these studies are threefold:

- to eliminate singularities of general equations by considering each case that may conduct to singularity,
- to estimate the parameters with more robustness using a simplified model (an adapted model gives more accuracy than the general one as shown in [18]),

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56 • to retrieve parameters that cannot be retrieved in
57 the general case because we eliminate some un-
58 knowns that are meaningless in the particular case
59 studied.

60 It is already known that the large number of par-
61 ticular cases prevent examining all the cases linearly.
62 In this paper, we introduce a new way to deal with
63 this amount of cases in three steps. (1) We eliminate,
64 with some simple rules, some redundant cases and
65 some physically impossible cases. (2) We divide the
66 set of cases into two sets, each corresponding to homo-
67 graphic or fundamental relations. (3) We divide again
68 the fundamental cases into sets corresponding to par-
69 ticular forms. We will provide details for each of these
70 steps in the following sections.

71 2. Stereo framework

72 In this section, we present the stereo framework and
73 the notations we will use in this paper.

74 2.1. Rigid displacements

75 We consider a rigid or piecewise rigid scene. A
76 3D-point $\mathbf{M} = [X Y Z 1]^T$ is moving onto $\mathbf{M}' =$
77 $[X' Y' Z' 1]^T$ by a rotation \mathbf{R} followed by a translation
78 $\mathbf{t} = [t_0 t_1 t_2]^T$:

$$79 \mathbf{M}' = \mathbf{R}\mathbf{M} + \mathbf{t}.$$

80 A rotation matrix \mathbf{R} depends only on three parameters
81 $\mathbf{r} = [r_0 r_1 r_2]^T$ related to the rotation angle θ and axis
82 \mathbf{u} by

$$83 \mathbf{r} = 2 \tan\left(\frac{1}{2}\theta\right)\mathbf{u} \Leftrightarrow \theta = 2 \arctan\left(\frac{1}{2}\|\mathbf{r}\|\right).$$

84 A rigid displacement is then parameterized by six pa-
85 rameters.

86 We note by $\tilde{\mathbf{r}}$ the antisymmetric matrix representing
87 the cross product $\mathbf{r} \wedge \cdot$:

$$88 \tilde{\mathbf{r}}\mathbf{x} = \mathbf{r} \wedge \mathbf{x} \quad \forall \mathbf{x}.$$

89 The rotation matrix $\mathbf{R} = e^{\mathbf{r}\wedge} = e^{\tilde{\mathbf{r}}}$ can be developed
90 as a rational Rodrigues formula [15]

$$91 \mathbf{R} = \mathbf{I} + \left[\frac{\tilde{\mathbf{r}} + (1/2)\tilde{\mathbf{r}}^2}{1 + \mathbf{r}^T \cdot \mathbf{r}/4} \right].$$

92 2.2. Camera projection

93 The most commonly camera model states that a
94 3D-point $\mathbf{M} = [X Y Z 1]^T$ is projected with a per-
95 spective projection onto an image plane on a 2D-point
96 $\mathbf{m} = [uv 1]^T$. In the reference frame attached to the
97 camera, the projection equation is

$$98 \mathbf{Z}\mathbf{m} = \underbrace{\begin{pmatrix} \alpha_u & \gamma & u_0 & 0 \\ 0 & \alpha_v & v_0 & 0 \\ 0 & 0 & 1 & 0 \end{pmatrix}}_{\mathbf{A}} \mathbf{M}, \quad (1)$$

99 where α_u and α_v represent the horizontal and verti-
100 cal lengths, u_0 and v_0 correspond to the image of the
101 optical center and γ is the skew factor. Those param-
102 eters are the intrinsic parameters and are collected in
103 the projection matrix \mathbf{A} .

104 2.3. Considering two frames

105 Let I_1 and I_2 denote two images. In the general
106 case, there exists a fundamental relation [7] between
107 points \mathbf{m}_2 in I_2 and points \mathbf{m}_1 in I_1 :

$$108 \mathbf{m}_2^T \mathbf{F} \mathbf{m}_1 = 0,$$

109 where \mathbf{F} is called the fundamental matrix and is related
110 to the intrinsic and extrinsic parameters by

$$111 \mathbf{F} = (\tilde{\mathbf{A}}_2 \mathbf{t}) \mathbf{A}_2 \mathbf{R} \mathbf{A}_1^{-1},$$

112 where \mathbf{A}_1 and \mathbf{A}_2 are the projection matrix for the first
113 and second frames, respectively, see (1).

114 This kind of relationship vanishes if the displace-
115 ment is a pure rotation or if the scene is planar. The
116 relation between points is homographic:

$$117 \mathbf{m}_2 = \mathbf{H} \mathbf{m}_1,$$

118 where \mathbf{H} is called the homographic matrix. Another
119 study on homographic matrices can be found in [11].

120 3. Deriving all particular cases

121 In order to study all particular cases of cameras,
122 object displacements and camera projection, we will
123 examine each particular value, considering each pa-
124 rameter at a time. A particular model is obtained by
125 combining several particular values.

126 3.1. Particular cases of intrinsic parameters

127 Authors generally make several hypotheses regard-
128 ing intrinsic parameters. For example, the most gen-
129 eral auto-calibration hypothesis states that the intrinsic
130 parameters are constant. They can be known or un-
131 known. However, usually, some parameters are con-
132 stant while others are not.

- 133 • The principal point of coordinates (u_0, v_0) can be
134 fixed and/or known in some cases (e.g. in the image
135 center), thus changing the reference frame, regard-
136 ing the principal point position.
- 137 • The γ parameter is usually assumed to be null or,
138 at least, considered to be a constant value.
- 139 • Enciso [6] has experimentally proven that for a large
140 number of cameras α_u/α_v can be considered to be
141 constant even if other intrinsic parameters change.
142 We express this as $f = \alpha_u = \alpha_v$.

143 Table 1 summarizes, for each intrinsic parameter,
144 the particular cases of interest (constant values are in-
145 dexed by zero). Subsequently, we will refer to each
146 case by the label given in the first column. For exam-
147 ple, g1 means that the γ parameter is null.

148 3.2. Particular cases of displacement

149 3.2.1. Discrete motion–continuous motion

150 In an image sequence, if the displacement between
151 two frames is small, we can approximate the rotation
152 equations by their first order:

$$153 \mathbf{R} = e^{\tilde{\mathbf{r}}} = \mathbf{I} + \tilde{\mathbf{r}} + o(\tilde{\mathbf{r}})$$

Table 1
Table of particular cases of intrinsic parameters for two frames

g1	$\gamma = 0$	γ constant and null
g2	$\gamma = \gamma_0$	γ constant
g3	$\gamma = \gamma(\tau)$	γ free
s1	$\alpha_u = \alpha_v(\tau)$	α_u/α_v constant and known
s2	$\alpha_u = \alpha_u(\tau)$	α_u free
f1	$\alpha_v = 1$	α_v constant and known
f2	$\alpha_v = f_0$	α_v constant
f3	$\alpha_v = \alpha_v(\tau)$	α_v free
c1	$u_0 = v_0 = 0$	u_0 and v_0 constant and known
c2	$u_0 = u_{0_0}$ and $v_0 = v_{0_0}$	u_0 and v_0 constant
c3	$u_0 = u_0(\tau)$ and $v_0 = v_0(\tau)$	u_0 and v_0 free

154 which occurs frequently in images sequences except
155 with high speed objects.

156 If the motion is larger, we can also consider the
157 second order expansion

$$158 \mathbf{R} = \mathbf{I} + \tilde{\mathbf{r}} + \frac{1}{2}\tilde{\mathbf{r}}^2 + o(\tilde{\mathbf{r}}^2).$$

159 3.2.2. About extrinsic parameters

160 The rotation parameters are related to the rotation
161 axis and the rotation angle by $\mathbf{r} = 2 \tan(\theta/2)\mathbf{u}$, where
162 \mathbf{u} is a unitary vector giving the direction of the rotation
163 axis.

164 Some components of \mathbf{u} can be known or null. Some
165 value of θ may yield singularities; $\theta = \pi/4$ and the
166 rotation axis is parallel to the translation vector for a
167 screw displacement.

168 Some robotic systems give precise values of the
169 robot displacements (angle, axis, translation). Some
170 values may be known (we denote by θ_0 a constant and
171 known value of a parameter θ). Other informations
172 regarding parallelism or orthogonality to a known di-
173 rection or to an other vector may also be available:

- 174 • the rotation axis is orthogonal to the translation
175 plane (e.g. planar motion):

$$176 \mathbf{r} \perp \mathbf{t} \Leftrightarrow \mathbf{r} \cdot \mathbf{t} = 0,$$

- 177 • screw displacement:

$$178 \mathbf{r} \parallel \mathbf{t} \Leftrightarrow \exists \kappa / \mathbf{r} = \kappa \mathbf{t}.$$

179 3.2.3. All constraints on motion

180 All these constraints, also called “atomic particu-
181 lar cases”, have simple expressions that can be easily
182 combined. In this purpose, we use the fact that \mathbf{u} is
183 a unitary vector and that, for monocular systems, the
184 norm of translation cannot be recovered. To parame-
185 terize these vectors with only two parameters, we di-
186 vide each component by a non-zero component. Then,
187 the dot product and scalar product induce linear rela-
188 tions. For example, $t_2 = 1$ and $\mathbf{t} \perp \mathbf{r}$ are equivalent
189 to $t_0u_0 + t_1u_1 + u_2 = 0 \Rightarrow u_2 = -t_0u_0 - t_1u_1$. All
190 cases are collected in Table 2.

191 3.2.4. Generating all cases

192 All particular cases, each called a “molecular case”,
193 are generated by combining the atomic cases and solv-

Table 2
Table of particular cases of displacements

u1	$u_0 = u_2 = 0, u_1 = 1$	Rotation axis \parallel y-axis	R1	$\mathbf{R} = \mathbf{I}$	Null rotation
u2	$u_0 = 0, u_1 = 1$	Rotation axis \perp x-axis	R2	$\mathbf{R} = \mathbf{I} + \tilde{\mathbf{r}}$	First order
u3	$u_2 = 0, u_1 = 1$	Rotation axis \perp z-axis	R3	$\mathbf{R} = \mathbf{I} + \tilde{\mathbf{r}} + \frac{1}{2}\tilde{\mathbf{r}}^2$	Second order
u4	$u_1 = 1$	General case	R4	$\mathbf{R} = \mathbf{I} + (\tilde{\mathbf{r}} + 1/2\tilde{\mathbf{r}}^2)/$ $(1 + \mathbf{r}^T\mathbf{r}/4)$	General case
u5	$u_0 = u_2 = 0, u_1 = -1$	Rotation axis \parallel y-axis			
u6	$u_0 = 0, u_1 = -1$	Rotation axis \perp x-axis	a1	$\theta = \pi/2$	Quarter turn
u7	$u_2 = 0, u_1 = -1$	Rotation axis \perp z-axis	a2	θ	Free angle
u8	$u_1 = -1$	General case			
u9	$u_0 = u_1 = 0, u_2 = 1$	Rotation axis \parallel z-axis	t1	$t_1 = t_2 = 0, t_0 = 1$	Translation \parallel x-axis
u10	$u_0 = 0, u_2 = 1$	Rotation axis \perp x-axis	t2	$t_1 = 0, t_0 = 1$	Translation \perp y-axis
u11	$u_1 = 0, u_2 = 1$	Rotation axis \perp y-axis	t3	$t_2 = 0, t_0 = 1$	Translation \perp z-axis
u12	$u_2 = 1$	General case	t4	$t_0 = 1$	General translation
u13	$u_0 = u_1 = 0, u_2 = -1$	Rotation axis \parallel z-axis	t5	$t_0 = t_2 = 0, t_1 = 1$	Translation \parallel z-axis
u14	$u_0 = 0, u_2 = -1$	Rotation axis \perp x-axis	t6	$t_0 = 0, t_1 = 1$	Translation \perp x-axis
u15	$u_1 = 0, u_2 = -1$	Rotation axis \perp y-axis	t7	$t_2 = 0, t_1 = 1$	Translation \perp z-axis
u16	$u_2 = -1$	General case	t8	$t_1 = 1$	General translation
u17	$u_1 = u_2 = 0, u_0 = 1$	Rotation axis \parallel x-axis	t9	$t_0 = t_1 = 0, t_2 = 1$	Translation \parallel z-axis
u18	$u_1 = 0, u_0 = 1$	Rotation axis \perp y-axis	t10	$t_0 = 0, t_2 = 1$	Translation \perp x-axis
u19	$u_2 = 0, u_0 = 1$	Rotation axis \perp z-axis	t11	$t_1 = 0, t_2 = 1$	Translation \perp y-axis
u20	$u_0 = 1$	General case	t12	$t_2 = 1$	General translation
u21	$u_1 = u_2 = 0, u_0 = -1$	Rotation axis \parallel x-axis			
u22	$u_1 = 0, u_0 = -1$	Rotation axis \perp y-axis	Z1	$\mathbf{t} \cdot \mathbf{u} = 0$	Translation \perp rotation axis
u23	$u_2 = 0, u_0 = -1$	Rotation axis \perp z-axis	Z2	$\mathbf{t} \wedge \mathbf{u} = 0$	Screw displacement
u24	$u_0 = -1$	General case	Z3		No relation

194 ing the constraints by a substitution.¹ A molecular
195 case is composed of one case in each family, a family
196 being named by a letter (g, s, f or c for projection
197 as seen in Table 1 and u, R, a, t or Z for motion as
198 seen in Table 2). Thus, a molecular case is identified
199 by the sequence:

201 $g[1-3]f[1-3]s[1-3]c[1-3]R[1-4]a[1-2]$
202 $u[1-24]t[1-12]z[1-3],$

203 where $g[1-3]$ means “one atomic case among g_1, g_2
204 and g_3 ”.

205 3.2.5. How many cases do we have?

206 If we look at the expression of the particular
207 above-mentioned cases, we obtain 6×10^6 particular
208 cases. However, this is not the real number because
209 of the incompatibility of some atomic cases and the
210 redundancy of some constraints. Two different sets of

atomic constraints can generate the same simplified
211 model. 212

It is easy to eliminate incompatible constraints. It
213 is not possible to deal with redundant constraints, be-
214 cause this requires to compare each set of combined
215 constraints with all others in order to determine the
216 similarity. The complexity of this process is $O(n^2)$. 217

Although we cannot remove redundant cases, we
218 propose an adapted strategy to deal with the large num-
219 ber of cases. The idea of this paper is: (i) to eliminate
220 some of the redundant cases by using some consider-
221 ations on the atomic cases and (ii) to limit the number
222 of cases by studying the particular forms of the matri-
223 ces. 224

225 3.2.6. Reducing the number of cases

Some redundancy are obvious 226

- In case (R1), one case of axis and angle is consid- 227
ered. 228
- In cases (R2) and (R3), we do not consider (a1) 229
when θ is equal to $\pi/2$. 230
- The case (a1) is only considered if $\mathbf{r} \parallel \mathbf{t}$, (Z2). 231

¹ This was done using Maple software for symbolic computa-
tions.

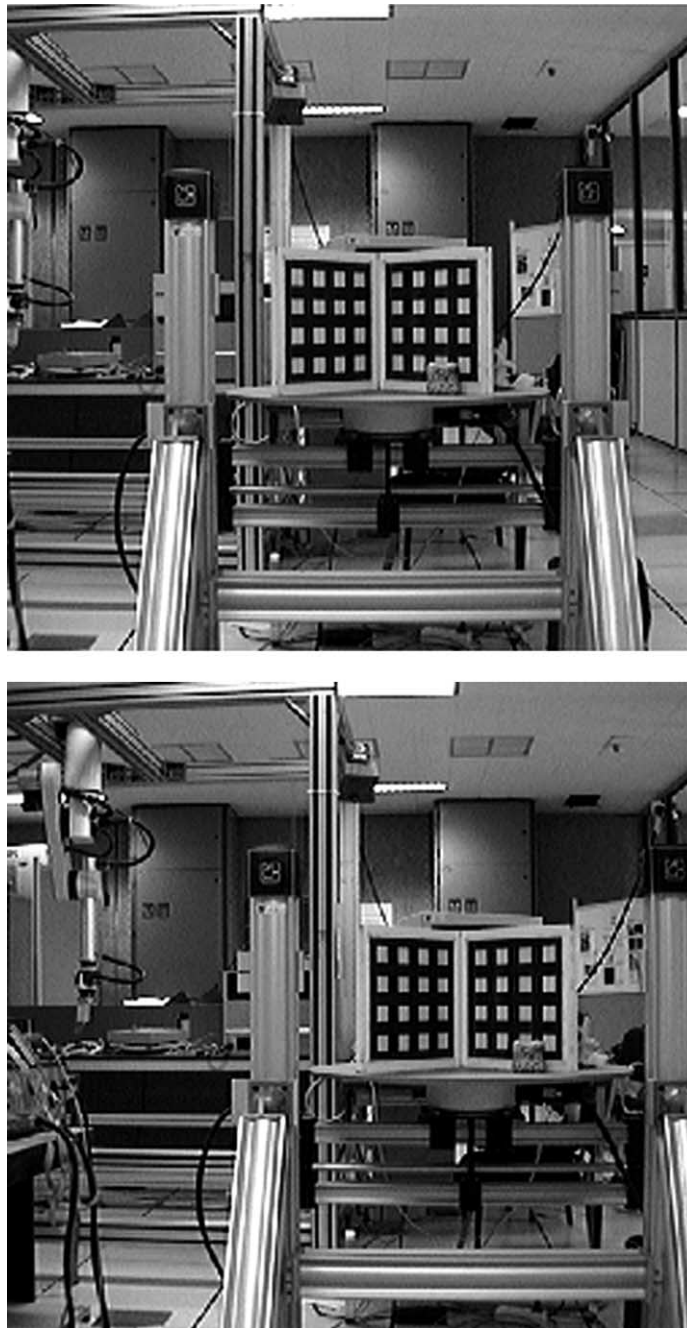


Fig. 1. Images for x -axis translation, small pan rotation and auto-focus.

232 This reduces the amount of cases of fundamental
233 relations to only 216 756 cases.

234 4. Forms of fundamental matrices

235 We have significantly reduced the number of cases
236 but this is not small enough to be computation-
237 ally tractable. We now split fundamental relations
238 in sets of matrices by forms. The matrix form is
239 determined using simple rules in order to obtain a
240 very simple parameterization. We consider (3×3)
241 matrices having nine parameters (coefficients). If a
242 coefficient is equal to zero, then there is one less
243 parameter. If a coefficient has the same expression
244 or is opposite to another, there is one less param-
245 eter again. These operations are very simple and
246 can be rapidly computed in each case. Furthermore,
247 we know that a fundamental matrix is defined up
248 to a scale factor, and that its determinant is fixed
249 to 0 (removing in most cases one parameter). This
250 process reduces the 216 756 cases to only 188 sub-
251 groups.

252 The table in Appendix A shows all the simpli-
253 fied forms obtained, and for each form, an exam-
254 ple of case that has generated it. This table will
255 be useful for people who want to implement the
256 algorithm.

257 5. Experiments

258 We have recorded several video sequences for
259 which the camera displacement induces a funda-
260 mental relation between image points \mathbf{m}_1 and \mathbf{m}_2 .
261 From each particular matrix form, we have estimated
262 the fundamental matrix parameters with the robust
263 least median square method in order to minimize
264 the distance between a 2D point \mathbf{m}_1 and its epipolar
265 line $\mathbf{F}\mathbf{m}_2$. To deal with cases with different degrees
266 of freedom, we use an appropriate Akaike criterion
267 [1].

268 For each recorded video sequence, we have veri-
269 fied that the model with the minimal residual error ef-
270 fectively corresponds to the displacement performed
271 by the robotic system. We present one experiment in
272 Fig. 1 for which the camera has performed a small
273 pan rotation followed by a translation parallel to the

x -axis. The auto-focus was also enabled. The case with
the minimal residual error corresponds to the funda-
mental matrix form number **59** in the table given in
Appendix A

$$\mathbf{F} = \begin{pmatrix} 0 & 0 & 0 \\ x_0 & x_1 & x_2 \\ 0 & -x_2 & x_3 \end{pmatrix}.$$

This particular form was obtained from cases where
the rotation was approximated to its first and second
order, the translation is parallel to the x -axis, the ro-
tation axis is orthogonal to the optical axis and the
intrinsic parameters are free.

284 6. Conclusion

In an earlier study on homographic matrices [11],
we have shown that it is possible to reduce the amount
of particular cases in order to make the case selection
computationally feasible. In this paper, we have shown
that a similar result can be obtained with fundamental
matrices using redundancies. We have experimentally
confirmed that our system is able to automatically se-
lect the case corresponding to the performed displace-
ment.

The applications are twofold: (i) an incremental
reconstruction of the scene and (ii) the segmen-
tation of objects moving with different displace-
ments or with different geometric properties in video
sequences.

This work has also been extended to mo-
tion estimation of human head inside MRI scan-
ner, improving the registration of fMRI volumes
[12].

303 Appendix A. Table of particular forms of 304 fundamental matrices

We denote by \mathbf{n}^o the form number, by \mathbf{p} the
number of parameters (we have not taken into ac-
count the fact that the fundamental matrix is de-
fined up to a scale factor and that $\det \mathbf{F} = 0$ but
we do so in our implementation) and by \mathbf{n} the
number of molecular cases that have generated a
form.

n°	p	Simplified form of fundamental matrix	For example generated by	n
1	1	[0 0 0 0 0 x ₆ 0 -x ₆ 0]	glf1slc1t1R1u24Z3a2	24
2	1	[0 0 x ₃ 0 0 0 -x ₃ 0 0]	glf1slc1t5R1u24Z3a2	4
3	1	[0 x ₂ 0 -x ₂ 0 0 0 0 0]	glf1slc1t9R1u24Z3a2	5
4	2	[0 0 0 0 0 x ₆ 0 -x ₆ x ₉]	glf1slc3t1R1u24Z3a2	12
5	2	[0 0 0 0 0 x ₆ 0 x ₈ 0]	glf3slc1t1R1u24Z3a2	6
6	2	[0 0 0 0 0 x ₆ x ₇ -x ₆ 0]	glf1slc1t1R2u13Z2a2	16
7	2	[0 0 0 0 x ₅ x ₆ 0 -x ₆ x ₅]	glf1slc1t1R2u17Z1a2	396
8	2	[0 0 0 x ₄ 0 0 x ₆ 0 -x ₆ 0]	glf1slc1t1R2u1Z2a2	16
9	2	[0 0 x ₃ 0 0 0 -x ₃ 0 x ₉]	glf1slc3t5R1u24Z3a2	2
10	2	[0 0 x ₃ 0 0 0 -x ₃ x ₈ 0]	glf1slc1t5R2u13Z2a2	8
11	2	[0 0 x ₃ 0 0 0 x ₇ 0 0]	glf1s2c1t5R1u24Z3a2	4
12	2	[0 0 x ₃ 0 0 x ₆ -x ₃ -x ₆ 0]	glf1slc1t3R1u24Z3a2	17
13	2	[0 x ₂ 0 -x ₂ 0 x ₆ 0 -x ₆ 0]	glf1slc1t11R1u24Z3a2	8
14	2	[0 x ₂ 0 -x ₂ 0 x ₆ 0 0 0]	glf1slc1t9R2u1Z2a2	24
15	2	[0 x ₂ 0 -x ₂ x ₅ 0 0 0 0]	g2f3slc1t9R1u24Z3a2	4
16	2	[0 x ₂ 0 x ₄ 0 0 0 0 0]	glf1s2c1t9R1u24Z3a2	3
17	2	[0 x ₂ x ₃ -x ₂ 0 0 -x ₃ 0 0]	glf1slc1t10R1u24Z3a2	4
18	2	[0 x ₂ x ₃ -x ₂ 0 0 0 0 0]	glf1slc1t9R2u17Z2a2	12
19	2	[0 x ₂ x ₃ 0 0 0 -x ₃ 0 0]	glf1slc1t5R2u17Z2a2	8
20	2	[x ₁ 0 x ₃ 0 0 0 -x ₃ 0 x ₁]	glf1slc1t5R2u1Z1a2	66
21	2	[x ₁ x ₂ 0 -x ₂ x ₁ 0 0 0 0]	glf1slc1t10R2u11Z1a2	198
22	3	[0 0 0 0 0 x ₆ 0 x ₈ x ₉]	glf3slc2t1R1u24Z3a2	12
23	3	[0 0 0 0 0 x ₆ x ₇ -x ₆ x ₉]	glf1slc2t1R2u13Z2a2	32
24	3	[0 0 0 0 0 x ₆ x ₇ x ₈ 0]	glf1slc1t1R3u13Z2a2	200
25	3	[0 0 0 0 x ₅ x ₆ 0 -x ₆ x ₉]	glf2slc1t1R2u17Z1a2	396
26	3	[0 0 0 0 x ₅ x ₆ x ₇ -x ₆ x ₅]	glf1slc1t1R2u11Z2a2	16
27	3	[0 0 0 x ₄ 0 x ₆ 0 x ₈ 0]	glf1slc1t1R3u1Z2a2	56
28	3	[0 0 0 x ₄ 0 x ₆ x ₇ -x ₆ 0]	glf1slc1t1R2u10Z2a2	32
29	3	[0 0 0 x ₄ x ₅ x ₆ 0 -x ₆ 0]	g2f1slc1t1R2u1Z2a2	32
30	3	[0 0 0 x ₄ x ₅ x ₆ 0 -x ₆ x ₅]	glf1slc1t1R2u19Z2a2	16
31	3	[0 0 x ₃ 0 0 0 -x ₃ x ₈ x ₉]	glf1slc2t5R2u13Z2a2	16
32	3	[0 0 x ₃ 0 0 0 x ₇ 0 x ₉]	glf1s2c2t5R1u24Z3a2	8
33	3	[0 0 x ₃ 0 0 0 x ₇ x ₈ 0]	glf1slc1t5R3u13Z2a2	64
34	3	[0 0 x ₃ 0 0 x ₆ -x ₃ -x ₆ x ₉]	glf1slc3t3R1u24Z3a2	13
35	3	[0 0 x ₃ 0 0 x ₆ -x ₃ x ₈ 0]	g2f1slc1t5R2u13Z2a2	22
36	3	[0 0 x ₃ 0 0 x ₆ x ₇ -x ₆ 0]	glf1s2c1t3R1u24Z3a2	4
37	3	[0 x ₂ 0 -x ₂ 0 x ₆ 0 x ₈ 0]	glf3slc1t11R1u24Z3a2	2
38	3	[0 x ₂ 0 -x ₂ x ₅ x ₆ 0 -x ₆ 0]	g3f1slc1t11R1u24Z3a2	4
39	3	[0 x ₂ 0 -x ₂ x ₅ x ₆ 0 0 0]	g2f3slc1t9R2u1Z2a2	12
40	3	[0 x ₂ 0 x ₄ 0 x ₆ 0 -x ₆ 0]	glf1s2c1t11R1u24Z3a2	4
41	3	[0 x ₂ 0 x ₄ 0 x ₆ 0 0 0]	glf1slc1t9R3u1Z2a2	60
42	3	[0 x ₂ 0 x ₄ x ₅ 0 0 0 0]	g2f1s2c1t9R1u24Z3a2	6
43	3	[0 x ₂ x ₃ -x ₂ 0 0 x ₇ 0 0]	glf3slc1t10R1u24Z3a2	2
44	3	[0 x ₂ x ₃ -x ₂ 0 x ₆ -x ₃ -x ₆ 0]	glf1slc1t12R1u24Z3a2	40
45	3	[0 x ₂ x ₃ -x ₂ 0 x ₆ 0 0 0]	glf1slc1t9R2u19Z2a2	60
46	3	[0 x ₂ x ₃ 0 0 0 -x ₃ x ₈ 0]	glf1slc1t5R2u11Z2a2	16

313 Appendix A (Continued)

n°	p	Simplified form of fundamental matrix	For example generated by	n
47	3	[0 x ₂ x ₃ 0 0 0 x ₇ 0 0]	g1f1s1c1t5R3u17Z2a2	64
48	3	[0 x ₂ x ₃ x ₄ 0 0 0 0 0]	g1f1s1c1t9R3u17Z2a2	60
49	3	[x ₁ 0 x ₃ 0 0 0 -x ₃ 0 x ₉]	g1f2s1c1t5R2u1Z1a2	66
50	3	[x ₁ 0 x ₃ 0 0 0 -x ₃ x ₈ x ₁]	g1f1s1c1t5R2u10Z2a2	8
51	3	[x ₁ x ₂ 0 -x ₂ x ₁ x ₆ 0 0 0]	g1f1s1c1t9R2u10Z2a2	24
52	3	[x ₁ x ₂ x ₃ -x ₂ x ₁ 0 0 0 0]	g1f1s1c1t9R2u11Z2a2	24
53	3	[x ₁ x ₂ x ₃ 0 0 0 -x ₃ 0 x ₁]	g1f1s1c1t5R2u19Z2a2	8
54	4	[0 0 0 0 0 x ₆ x ₇ x ₈ x ₉]	g1f1s1c2t1R3u13Z2a2	400
55	4	[0 0 0 0 x ₅ x ₆ 0 x ₈ x ₉]	g1f1s1c2t1R2u17Z1a2	2772
56	4	[0 0 0 0 x ₅ x ₆ x ₇ -x ₆ x ₉]	g1f2s1c1t1R2u11Z2a2	16
57	4	[0 0 0 0 x ₅ x ₆ x ₇ x ₈ x ₅]	g2f1s1c1t1R2u11Z2a2	32
58	4	[0 0 0 x ₄ 0 x ₆ x ₇ x ₈ 0]	g1f3s1c1t1R2u10Z2a2	16
59	4	[0 0 0 x ₄ x ₅ x ₆ 0 -x ₆ x ₉]	g1f2s1c1t1R2u19Z2a2	80
60	4	[0 0 0 x ₄ x ₅ x ₆ 0 x ₈ 0]	g2f1s1c1t1R3u1Z2a2	112
61	4	[0 0 0 x ₄ x ₅ x ₆ x ₇ -x ₆ x ₅]	g1f1s1c1t1R2u12Z2a2	24
62	4	[0 0 x ₃ 0 0 0 x ₇ x ₈ x ₉]	g1f1s1c2t5R3u13Z2a2	128
63	4	[0 0 x ₃ 0 0 x ₆ -x ₃ x ₈ x ₉]	g2f1s1c2t5R2u13Z2a2	44
64	4	[0 0 x ₃ 0 0 x ₆ x ₇ -x ₆ x ₉]	g1f1s2c2t3R1u24Z3a2	8
65	4	[0 0 x ₃ 0 0 x ₆ x ₇ x ₈ 0]	g1f1s1c1t3R2u13Z2a2	588
66	4	[0 x ₂ 0 -x ₂ x ₅ x ₆ 0 x ₈ 0]	g2f3s1c1t11R1u24Z3a2	4
67	4	[0 x ₂ 0 x ₄ 0 x ₆ 0 x ₈ 0]	g1f1s1c1t11R2u1Z2a2	146
68	4	[0 x ₂ 0 x ₄ x ₅ x ₆ 0 -x ₆ 0]	g2f1s2c1t11R1u24Z3a2	8
69	4	[0 x ₂ 0 x ₄ x ₅ x ₆ 0 0 0]	g2f1s1c1t9R3u1Z2a2	120
70	4	[0 x ₂ x ₃ -x ₂ 0 x ₆ -x ₃ -x ₆ x ₉]	g1f3s1c2t9R1u24Z3a2	9
71	4	[0 x ₂ x ₃ -x ₂ x ₅ x ₆ 0 -x ₆ x ₅]	g1f1s1c1t11R2u17Z2a2	8
72	4	[0 x ₂ x ₃ -x ₂ x ₅ x ₆ 0 0 0]	g2f3s1c1t9R2u17Z2a2	36
73	4	[0 x ₂ x ₃ 0 0 0 x ₇ x ₈ 0]	g1f1s2c1t5R2u11Z2a2	32
74	4	[0 x ₂ x ₃ 0 x ₅ x ₆ -x ₃ -x ₆ 0]	g2f1s1c1t5R2u17Z2a2	12
75	4	[0 x ₂ x ₃ 0 x ₅ x ₆ -x ₃ -x ₆ x ₅]	g1f1s1c1t3R2u17Z2a2	8
76	4	[0 x ₂ x ₃ x ₄ 0 0 x ₇ 0 0]	g1f1s1c1t10R2u17Z2a2	150
77	4	[0 x ₂ x ₃ x ₄ 0 x ₆ 0 0 0]	g1f1s2c1t9R2u19Z2a2	24
78	4	[x ₁ 0 x ₃ 0 0 0 -x ₃ x ₈ x ₉]	g1f2s1c1t5R2u10Z2a2	8
79	4	[x ₁ 0 x ₃ 0 0 0 x ₇ 0 x ₉]	g1f1s1c2t5R2u1Z1a2	1056
80	4	[x ₁ 0 x ₃ x ₄ 0 x ₆ -x ₃ -x ₆ x ₁]	g1f1s1c1t3R2u1Z2a2	8
81	4	[x ₁ x ₂ 0 -x ₂ x ₁ x ₆ x ₇ -x ₆ 0]	g1f1s1c1t11R2u13Z2a2	16
82	4	[x ₁ x ₂ 0 x ₄ x ₅ 0 0 0 0]	g1f1s2c1t10R2u11Z1a2	990
83	4	[x ₁ x ₂ x ₃ -x ₂ 0 x ₆ -x ₃ 0 x ₁]	g1f1s1c1t10R2u1Z2a2	8
84	4	[x ₁ x ₂ x ₃ -x ₂ x ₁ 0 -x ₃ x ₈ 0]	g1f1s1c1t10R2u13Z2a2	16
85	4	[x ₁ x ₂ x ₃ -x ₂ x ₁ x ₆ 0 0 0]	g1f1s1c1t9R2u12Z2a2	36
86	4	[x ₁ x ₂ x ₃ 0 0 0 -x ₃ 0 x ₉]	g1f2s1c1t5R2u19Z2a2	8
87	4	[x ₁ x ₂ x ₃ 0 0 0 -x ₃ x ₈ x ₁]	g1f1s1c1t5R2u12Z2a2	12
88	5	[0 0 0 0 x ₅ x ₆ x ₇ x ₈ x ₉]	g1f1s1c2t1R2u11Z2a2	368
89	5	[0 0 0 x ₄ 0 x ₆ x ₇ x ₈ x ₉]	g1f1s1c2t1R2u10Z2a2	240
90	5	[0 0 0 x ₄ x ₅ x ₆ 0 x ₈ x ₉]	g1f3s1c1t1R2u19Z2a2	48

315 Appendix A (Continued)

n°	p	Simplified form of fundamental matrix									For example generated by	n
91	5	[0	0	0	x_4	x_5	x_6	x_7	$-x_6$	x_9]	g1f2s1c1t1R2u12Z2a2	24
92	5	[0	0	0	x_4	x_5	x_6	x_7	x_8	$-x_5$]	g1f1s1c1t1R3u10Z2a2	32
93	5	[0	0	0	x_4	x_5	x_6	x_7	x_8	0]	g2f1s1c1t1R2u10Z2a2	96
94	5	[0	0	0	x_4	x_5	x_6	x_7	x_8	x_5]	g1f1s1c1t1R3u11Z2a2	64
95	5	[0	0	x_3	0	0	x_6	x_7	x_8	x_9]	g1f1s1c2t3R2u13Z2a2	1176
96	5	[0	x_2	0	x_4	x_5	x_6	0	x_8	0]	g2f1s1c1t11R2u1Z2a2	292
97	5	[0	x_2	x_3	$-x_2$	0	x_6	$-x_3$	x_8	x_9]	g1f1s1c2t9R2u1Z2a2	26
98	5	[0	x_2	x_3	$-x_2$	0	x_6	x_7	$-x_6$	x_9]	g1f1s1c2t9R2u17Z2a2	14
99	5	[0	x_2	x_3	$-x_2$	0	x_6	x_7	x_8	0]	g1f3s1c1t12R1u24Z3a2	3
100	5	[0	x_2	x_3	$-x_2$	x_5	x_6	$-x_3$	x_8	0]	g3f1s1c1t10R1u24Z3a2	10
101	5	[0	x_2	x_3	$-x_2$	x_5	x_6	0	$-x_6$	x_9]	g1f2s1c1t11R2u17Z2a2	8
102	5	[0	x_2	x_3	$-x_2$	x_5	x_6	0	x_8	x_5]	g2f1s1c1t11R2u17Z2a2	12
103	5	[0	x_2	x_3	0	0	0	x_7	x_8	x_9]	g1f1s1c2t5R2u11Z2a2	240
104	5	[0	x_2	x_3	0	x_5	x_6	$-x_3$	$-x_6$	x_9]	g1f2s1c1t3R2u17Z2a2	32
105	5	[0	x_2	x_3	0	x_5	x_6	$-x_3$	x_8	0]	g2f1s1c1t5R2u11Z2a2	36
106	5	[0	x_2	x_3	0	x_5	x_6	x_7	$-x_6$	x_5]	g1f1s1c1t3R3u17Z2a2	40
107	5	[0	x_2	x_3	x_4	0	x_6	x_7	$-x_6$	0]	g1f1s2c1t12R1u24Z3a2	6
108	5	[0	x_2	x_3	x_4	x_5	x_6	0	$-x_6$	x_5]	g1f1s1c1t11R3u17Z2a2	40
109	5	[0	x_2	x_3	x_4	x_5	x_6	0	0	0]	g2f1s1c1t9R3u17Z2a2	168
110	5	[x_1	0	x_3	0	0	0	x_7	x_8	x_9]	g1f1s1c2t5R2u10Z2a2	128
111	5	[x_1	0	x_3	x_4	0	x_6	$-x_3$	$-x_6$	x_9]	g1f2s1c1t3R2u1Z2a2	8
112	5	[x_1	0	x_3	x_4	0	x_6	$-x_3$	x_8	x_1]	g1f1s1c1t3R3u1Z2a2	16
113	5	[x_1	x_2	0	$-x_2$	x_1	x_6	x_7	x_8	0]	g1f1s1c1t11R3u13Z2a2	56
114	5	[x_1	x_2	0	x_4	x_5	x_6	0	0	0]	g1f1s2c1t9R2u10Z2a2	120
115	5	[x_1	x_2	x_3	$-x_2$	0	x_6	$-x_3$	0	x_9]	g1f2s1c1t10R2u1Z2a2	8
116	5	[x_1	x_2	x_3	$-x_2$	x_1	0	x_7	x_8	0]	g1f1s1c1t10R3u13Z2a2	56
117	5	[x_1	x_2	x_3	0	0	0	$-x_3$	x_8	x_9]	g1f2s1c1t5R2u12Z2a2	12
118	5	[x_1	x_2	x_3	0	0	0	x_7	0	x_9]	g1f1s2c1t5R2u19Z2a2	32
119	5	[x_1	x_2	x_3	0	0	0	x_7	x_8	$-x_1$]	g1f1s1c1t5R3u11Z2a2	16
120	5	[x_1	x_2	x_3	0	0	0	x_7	x_8	x_1]	g1f1s1c1t5R3u10Z2a2	32
121	5	[x_1	x_2	x_3	x_2	x_5	x_6	$-x_3$	$-x_6$	x_1]	g2f1s1c1t5R2u1Z1a2	70
122	5	[x_1	x_2	x_3	x_4	$-x_1$	x_6	0	0	0]	g1f1s1c1t9R3u19Z2a2	48
123	5	[x_1	x_2	x_3	x_4	0	x_6	$-x_3$	0	x_1]	g1f1s1c1t10R3u1Z2a2	16
124	5	[x_1	x_2	x_3	x_4	x_1	x_6	0	0	0]	g1f1s1c1t9R3u10Z2a2	96
125	5	[x_1	x_2	x_3	x_4	x_5	0	0	0	0]	g1f1s2c1t9R2u11Z2a2	24
126	6	[0	0	0	x_4	x_5	x_6	x_7	x_8	x_9]	g1f1s1c1t1R3u12Z2a2	5160
127	6	[0	x_2	x_3	$-x_2$	0	x_6	x_7	x_8	x_9]	g1f1s1c2t9R2u19Z2a2	199
128	6	[0	x_2	x_3	$-x_2$	x_5	x_6	$-x_3$	x_8	x_9]	g2f3s1c2t11R1u24Z3a2	34
129	6	[0	x_2	x_3	$-x_2$	x_5	x_6	0	x_8	x_9]	g1f3s1c1t11R2u17Z2a2	44
130	6	[0	x_2	x_3	$-x_2$	x_5	x_6	x_7	x_8	0]	g2f3s1c1t10R1u24Z3a2	10
131	6	[0	x_2	x_3	0	x_5	x_6	$-x_3$	x_8	x_9]	g3f1s1c1t3R2u17Z2a2	8
132	6	[0	x_2	x_3	0	x_5	x_6	x_7	$-x_6$	x_9]	g1f2s1c1t3R3u17Z2a2	40
133	6	[0	x_2	x_3	0	x_5	x_6	x_7	x_8	0]	g2f1s1c1t5R3u17Z2a2	192
316 134	6	[0	x_2	x_3	0	x_5	x_6	x_7	x_8	x_5]	g1f1s1c1t3R2u11Z2a2	32

317 Appendix A (Continued)

n°	p	Simplified form of fundamental matrix	For example generated by	n
135	6	$[0 \ x_2 \ x_3 \ x_4 \ 0 \ x_6 \ x_7 \ x_8 \ 0]$	g1f3s2c1t12R1u24Z3a2	3
136	6	$[0 \ x_2 \ x_3 \ x_4 \ x_5 \ x_6 \ 0 \ -x_6 \ x_9]$	g1f2s1c1t11R3u17Z2a2	40
137	6	$[0 \ x_2 \ x_3 \ x_4 \ x_5 \ x_6 \ 0 \ x_8 \ x_5]$	g1f1s1c1t11R2u19Z2a2	32
138	6	$[0 \ x_2 \ x_3 \ x_4 \ x_5 \ x_6 \ x_7 \ -x_6 \ x_5]$	g1f1s1c1t12R2u17Z2a2	84
139	6	$[x_1 \ 0 \ x_3 \ x_4 \ 0 \ x_6 \ -x_3 \ x_8 \ x_9]$	g1f2s1c1t3R3u1Z2a2	16
140	6	$[x_1 \ 0 \ x_3 \ x_4 \ 0 \ x_6 \ x_7 \ -x_6 \ x_9]$	g1f1s2c1t3R2u1Z2a2	16
141	6	$[x_1 \ 0 \ x_3 \ x_4 \ 0 \ x_6 \ x_7 \ -x_6 \ x_9]$	g1f2s2c1t6R2u5Z3a2	16
142	6	$[x_1 \ x_2 \ 0 \ x_4 \ x_1 \ x_6 \ x_7 \ x_8 \ 0]$	g1f1s1c1t11R2u10Z2a2	48
143	6	$[x_1 \ x_2 \ 0 \ x_4 \ x_5 \ x_6 \ x_7 \ -x_6 \ 0]$	g1f1s2c1t11R2u13Z2a2	16
144	6	$[x_1 \ x_2 \ x_3 \ -x_2 \ 0 \ x_6 \ x_7 \ 0 \ x_9]$	g1f3s1c1t10R2u1Z2a2	8
145	6	$[x_1 \ x_2 \ x_3 \ -x_2 \ x_1 \ x_6 \ x_7 \ x_8 \ 0]$	g1f1s1c1t12R2u13Z2a2	126
146	6	$[x_1 \ x_2 \ x_3 \ -x_2 \ x_5 \ x_6 \ -x_3 \ x_6 \ x_9]$	g1f1s1c1t10R2u10Z1a2	144
147	6	$[x_1 \ x_2 \ x_3 \ -x_2 \ x_5 \ x_6 \ x_3 \ -x_6 \ x_9]$	g1f1s1c1t11R2u11Z1a2	144
148	6	$[x_1 \ x_2 \ x_3 \ 0 \ 0 \ 0 \ x_7 \ x_8 \ x_9]$	g1f1s1c1t5R3u1Z2a2	1536
149	6	$[x_1 \ x_2 \ x_3 \ x_2 \ x_5 \ x_6 \ -x_3 \ -x_6 \ x_9]$	g1f1s1c1t3R2u19Z1a2	358
150	6	$[x_1 \ x_2 \ x_3 \ x_2 \ x_5 \ x_6 \ -x_3 \ x_8 \ x_1]$	g2f1s1c1t5R2u10Z2a2	12
151	6	$[x_1 \ x_2 \ x_3 \ x_4 \ 0 \ x_6 \ -x_3 \ 0 \ x_9]$	g1f2s1c1t10R3u1Z2a2	16
152	6	$[x_1 \ x_2 \ x_3 \ x_4 \ 0 \ x_6 \ -x_3 \ x_8 \ x_1]$	g1f1s1c1t12R2u1Z2a2	42
153	6	$[x_1 \ x_2 \ x_3 \ x_4 \ 0 \ x_6 \ x_7 \ 0 \ x_1]$	g1f1s1c1t10R2u19Z2a2	16
154	6	$[x_1 \ x_2 \ x_3 \ x_4 \ x_1 \ 0 \ x_7 \ x_8 \ 0]$	g1f1s1c1t10R2u11Z2a2	48
155	6	$[x_1 \ x_2 \ x_3 \ x_4 \ x_5 \ x_6 \ -x_3 \ -x_6 \ x_1]$	g2f1s1c1t3R2u1Z2a2	24
156	6	$[x_1 \ x_2 \ x_3 \ x_4 \ x_5 \ x_6 \ 0 \ 0 \ 0]$	g1f1s1c1t9R3u1Z2a2	1428
157	7	$[0 \ x_2 \ x_3 \ -x_2 \ x_5 \ x_6 \ x_7 \ x_8 \ x_9]$	g1f1s1c2t11R2u17Z2a2	270
158	7	$[0 \ x_2 \ x_3 \ 0 \ x_5 \ x_6 \ x_7 \ x_8 \ x_9]$	g1f1s1c2t3R2u11Z2a2	2480
159	7	$[0 \ x_2 \ x_3 \ x_4 \ 0 \ x_6 \ x_7 \ x_8 \ x_9]$	g1f1s1c2t10R2u17Z2a2	912
160	7	$[0 \ x_2 \ x_3 \ x_4 \ x_5 \ x_6 \ 0 \ x_8 \ x_9]$	g1f2s1c1t11R2u19Z2a2	536
161	7	$[0 \ x_2 \ x_3 \ x_4 \ x_5 \ x_6 \ x_7 \ -x_6 \ x_9]$	g1f2s1c1t12R2u17Z2a2	84
162	7	$[0 \ x_2 \ x_3 \ x_4 \ x_5 \ x_6 \ x_7 \ x_8 \ 0]$	g2f1s1c1t10R2u17Z2a2	318
163	7	$[x_1 \ 0 \ x_3 \ x_4 \ 0 \ x_6 \ x_7 \ x_8 \ x_9]$	g1f1s1c2t3R2u10Z2a2	640
164	7	$[x_1 \ x_2 \ 0 \ x_4 \ x_5 \ x_6 \ x_7 \ x_8 \ 0]$	g1f1s2c1t11R2u10Z2a2	584
165	7	$[x_1 \ x_2 \ x_3 \ -x_2 \ 0 \ x_6 \ x_7 \ x_8 \ x_9]$	g1f1s1c2t10R2u1Z2a2	48
166	7	$[x_1 \ x_2 \ x_3 \ -x_2 \ x_1 \ x_6 \ x_7 \ x_8 \ x_9]$	g1f1s1c2t10R2u11Z1a2	1104
167	7	$[x_1 \ x_2 \ x_3 \ -x_2 \ x_5 \ x_6 \ -x_3 \ x_8 \ x_9]$	g1f1s1c1t10R2u10Z2a2	32
168	7	$[x_1 \ x_2 \ x_3 \ -x_2 \ x_5 \ x_6 \ x_7 \ -x_6 \ x_9]$	g1f1s1c1t11R2u11Z2a2	32
169	7	$[x_1 \ x_2 \ x_3 \ x_2 \ x_5 \ x_6 \ -x_3 \ x_8 \ x_9]$	g2f2s1c1t5R2u10Z2a2	12
170	7	$[x_1 \ x_2 \ x_3 \ x_4 \ 0 \ x_6 \ -x_3 \ x_8 \ x_9]$	g1f2s1c1t12R2u1Z2a2	42
171	7	$[x_1 \ x_2 \ x_3 \ x_4 \ 0 \ x_6 \ x_7 \ 0 \ x_9]$	g1f1s2c1t10R2u19Z2a2	168
172	7	$[x_1 \ x_2 \ x_3 \ x_4 \ x_5 \ 0 \ x_7 \ x_8 \ 0]$	g1f1s2c1t10R2u11Z2a2	120
173	7	$[x_1 \ x_2 \ x_3 \ x_4 \ x_5 \ x_6 \ -x_3 \ -x_6 \ x_9]$	g1f1s1c1t3R2u19Z2a2	104
174	7	$[x_1 \ x_2 \ x_3 \ x_4 \ x_5 \ x_6 \ -x_3 \ x_8 \ 0]$	g2f1s1c1t10R2u13Z2a2	32
175	7	$[x_1 \ x_2 \ x_3 \ x_4 \ x_5 \ x_6 \ -x_3 \ x_8 \ x_1]$	g2f1s1c1t10R2u1Z2a2	262
176	8	$[0 \ x_2 \ x_3 \ x_4 \ x_5 \ x_6 \ x_7 \ x_8 \ x_9]$	g1f1s1c2t11R2u19Z2a2	5220
177	8	$[x_1 \ x_2 \ x_3 \ -x_2 \ x_5 \ x_6 \ x_7 \ x_8 \ x_9]$	g1f1s1c2t10R2u10Z1a2	1232
318 178	8	$[x_1 \ x_2 \ x_3 \ x_2 \ x_5 \ x_6 \ x_7 \ x_8 \ x_9]$	g1f1s1c2t3R2u19Z1a2	1564

319 Appendix A (*Continued*)

n°	p	Simplified form of fundamental matrix	For example generated by	n
179	8	$[x_1 \ x_2 \ x_3 \ x_4 \ -x_1 \ x_6 \ x_7 \ x_8 \ x_9]$	g1f1s1c2t9R3u19Z2a2	96
180	8	$[x_1 \ x_2 \ x_3 \ x_4 \ 0 \ x_6 \ x_7 \ x_8 \ x_9]$	g1f1s1c2t10R2u19Z2a2	1104
181	8	$[x_1 \ x_2 \ x_3 \ x_4 \ x_1 \ x_6 \ x_7 \ x_8 \ x_9]$	g1f1s1c2t10R2u11Z2a2	384
182	8	$[x_1 \ x_2 \ x_3 \ x_4 \ x_5 \ x_6 \ -x_3 \ x_8 \ x_9]$	g2f1s1c1t10R2u10Z1a2	774
183	8	$[x_1 \ x_2 \ x_3 \ x_4 \ x_5 \ x_6 \ x_3 \ x_8 \ x_9]$	g2f1s1c1t11R2u11Z1a2	288
184	8	$[x_1 \ x_2 \ x_3 \ x_4 \ x_5 \ x_6 \ x_7 \ -x_6 \ x_9]$	g1f1s2c1t11R2u11Z1a2	352
185	8	$[x_1 \ x_2 \ x_3 \ x_4 \ x_5 \ x_6 \ x_7 \ x_6 \ x_9]$	g1f1s2c1t10R2u10Z1a2	144
186	8	$[x_1 \ x_2 \ x_3 \ x_4 \ x_5 \ x_6 \ x_7 \ x_8 \ -x_1]$	g2f1s1c1t5R3u11Z2a2	32
187	8	$[x_1 \ x_2 \ x_3 \ x_4 \ x_5 \ x_6 \ x_7 \ x_8 \ 0]$	g1f1s2c1t12R2u13Z2a2	1078
188	8	$[x_1 \ x_2 \ x_3 \ x_4 \ x_5 \ x_6 \ x_7 \ x_8 \ x_1]$	g2f1s1c1t10R2u19Z2a2	128

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